

# Impact of hybrid electric aircraft on contrail formation

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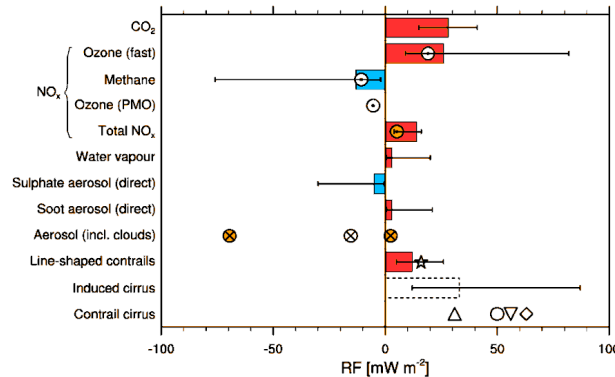
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3<sup>rd</sup> ECATS conference, 13<sup>th</sup>-15<sup>th</sup> October, 2020

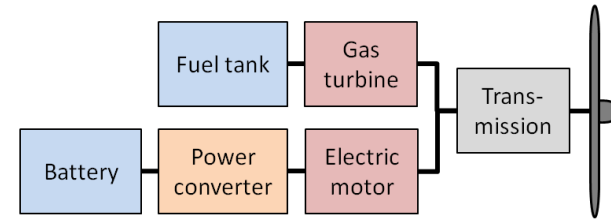


# Introduction

- Aviation contributes 5% to the anthropogenic warming effects
- Contrails' effects are short but large
- Operational flexibility of parallel hybrid electric concept provides possibility to reduce contrail formation in contrail-sensitive regions



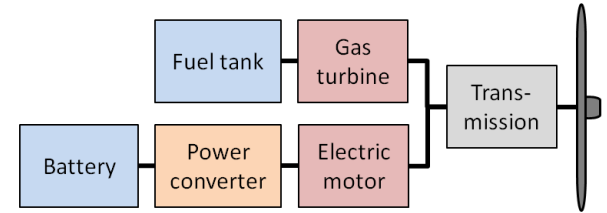
○ Sévde et al. (2014): EMAC, multi-model mean      △ Burkhardt and Kärcher (2011)  
 ⊗ Righi et al. (2013): reference case, parameter span      ○ Schumann and Graf (2013)  
 ☆ Voigt et al. (2011)      ◇ Schumann et al. (2015)  
    ▽ Bock and Burkhardt (2016)



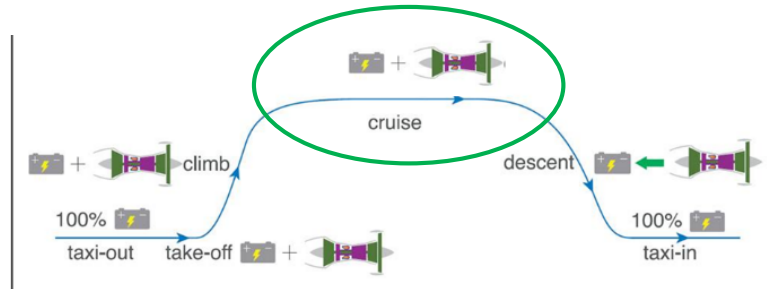
Parallel architecture

# Baseline aircraft/engine

- Airbus A320neo type
- CFM LEAP-1A engine
- Technology level 2030 for electric system
- Cruise condition with given thrust



Parameter:	2030
Battery energy density	600 Wh/kg
Maximum electric motor efficiency	97.5%



# Methodology overview

## Inputs

Hybrid electric aircraft (HEA):

- Turbofan engine
- 2030 battery technology
- Power management strategy



## EMAC/CONTRAIL submodel\*

Derive Schmidt Appleman Criterion (SAC) for HEA

Calculate potential contrail coverage (PCC) vs. hybridization



Earth system model (EMAC)\*\*:

- Horizontal grid of 310 km
- Vertical resolution of 1 km
- Time step 12 mins

## Results

Analyze changes of PCC by HEA:

- Local effects
- Climatological effects
- Seasonal effects

\*supplement of Grewe et al., 2014

\*\*Jöckel et al. 2010

# Derivation of Schmidt Appleman Criterion for HEA

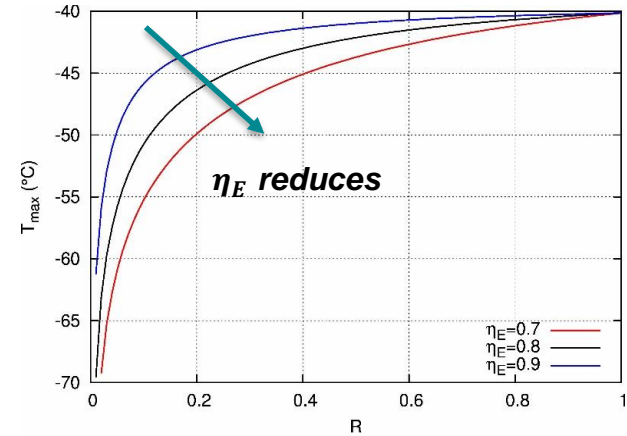
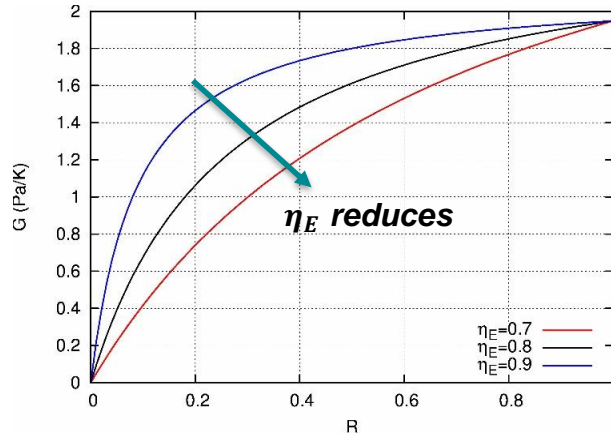
$$F \cdot V = \underbrace{\eta_k \cdot \dot{m}_f \cdot Q}_{\text{Kerosene}} + \underbrace{\eta_E \cdot P_E}_{\text{Electricity}}$$

$$G = \frac{c_p p_a}{\varepsilon} \frac{R \cdot EI_{H_2O}}{R \cdot (1 - \eta_k) Q + (1 - R)(1 - \eta_E) Q_E^0}$$

$$R := \frac{\dot{m}_f}{\dot{m}_{fmax}}, Q_E^0 := Q(\eta_k / \eta_E)$$

Variable	Value	Variable	Value
Baseline propulsion efficiency ( $\eta_k$ )	0.4	Water emission index (EI <sub>H2O</sub> )	1.25
Lower heating value (Q), MJ/kg	43.2	Molar mass ration of water vapor and dry air ( $\varepsilon$ )	0.622

# Threshold of contrail formation by SAC at 250 hPa

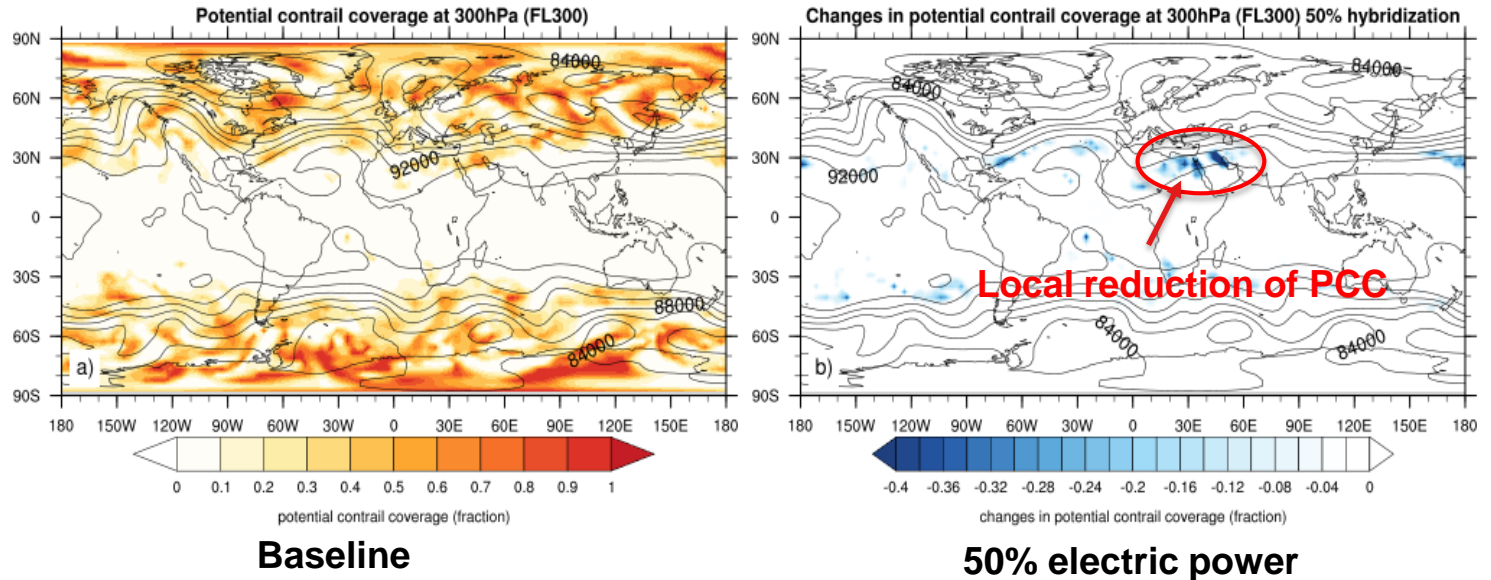


Pure electric  
propulsion

Pure kerosene  
propulsion

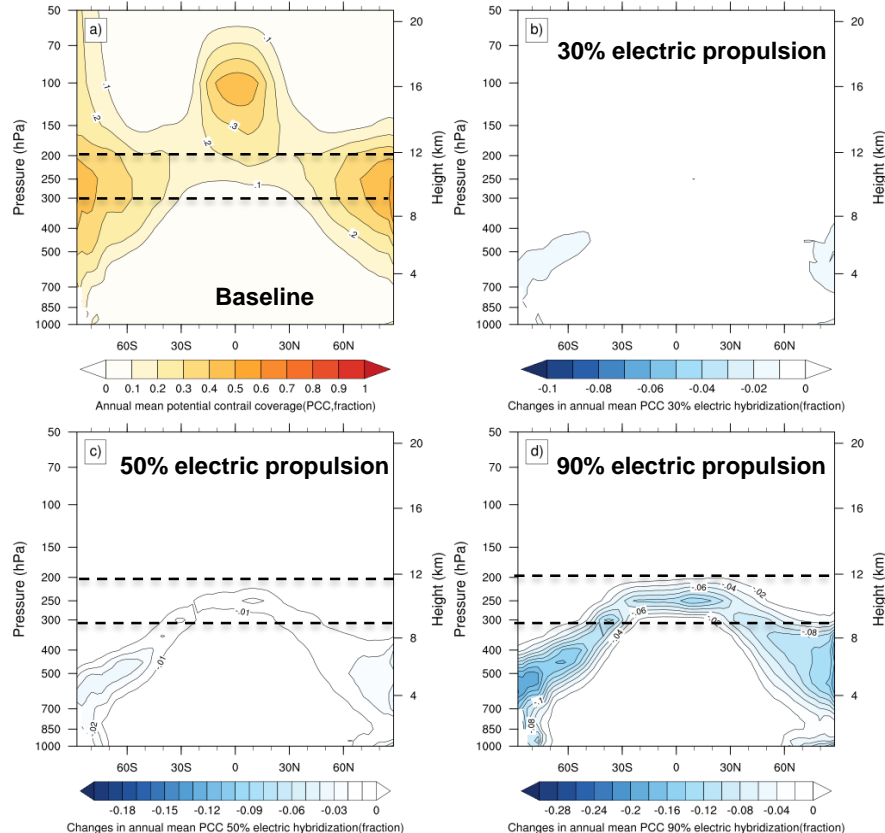
- $\eta_E$  is the efficiency of the electrical powertrain
- The slope ( $G$ ) decreases as increasing the electrical power
- The temperature threshold ( $T_{max}$ ) of HEA to form contrails reduces as increasing the electrical power
- In most situations, a large percentage of electric power is required for contrail avoidance

# Local changes of potential contrail coverage (PCC)



- At FL300, 50% hydration: the reduction in PCC is at 30°N and 40°S and localized

# Climatological effects on PCC



- Annual mean of one year simulation results
- Figure a)->d): baseline aircraft->30%->50%->90%
- Hybrid electric aircraft tends to form contrails at higher altitude



# Conclusions

- The operational flexibility of hybrid-electric aircraft (HEA) offers opportunities in contrail avoidance.
- The HEA requires lower atmospheric temperatures to form contrails than the conventional aircraft.
- To avoid contrails at cruise altitude, a large fraction of electric power (more than 50% in the current study) is required.
- The reduction in PCC can be achieved locally.

# Discussions and future work

- The current work doesn't not consider the actual flight routes, which will be included in the subsequent research
- The derivation of SAC is valid for hybrid electric system with battery. For other forms of hybridization, e.g., fuel cell, a different SAC should be derived
- In case of designing a HEA system for contrail avoidance, a proper power management strategy is required at the first place.

Thank you!  
Questions?